



# BIOMEDICAL ANTHROPOMETRIC EVALUATION AND CONCEPTUAL MECHANICAL DESIGN OF A ROBOTIC SYSTEM FOR LOWER LIMBS PASSIVE-REHABILITATION ON POST-STROKE PATIENTS

EVALUACIÓN ANTROPOMÉTRICA BIOMÉDICA Y DISEÑO MECÁNICO CONCEPTUAL DE UN SISTEMA ROBÓTICO PARA LA REHABILITACIÓN PASIVA DE MIEMBROS INFERIORES EN PACIENTES POST-ACCIDENTE CEREBROVASCULAR

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## ABSTRACT

**Background:** Cerebrovascular accident (CVA) is one of the main causes of permanent disability, as it can cause serious brain injuries with significant physical consequences, limiting the ability to perform daily activities. **Objective:** This research aimed to design a robotic system of passive-continuous movement for the rehabilitation of lower limbs in adult patients with stroke, thus improving the chances of recovery of their walking mobility. **Methods:** Modeling and simulation of the robotic system using Computer Aided Design (CAD), using the engineering software Autodesk Inventor Professional 2023. **Results:** The initial and final positions of the robotic system were obtained, as well as the simulation of passive-continuous movement. **Conclusions:** Taking precise measurements of a patient maximizes the possibility of implementing a functional prototype that contributes to the rehabilitation process.

**Keywords:** Robotics; Rehabilitation; Lower Limbs; Design; Cerebrovascular Accident; Simulation. (Source: MESH-NLM)

## RESUMEN

**Antecedentes:** El accidente cerebrovascular (ACV) es una de las principales causas de discapacidad permanente, ya que puede provocar lesiones cerebrales graves con secuelas físicas significativas, limitando la capacidad de realizar actividades diarias. **Objetivo:** Esta investigación tuvo como objetivo diseñar un sistema robótico de movimiento pasivo-continuo para la rehabilitación de miembros inferiores en pacientes adultos con ACV, mejorando así las probabilidades de recuperación de su movilidad de marcha. **Metodología:** Se llevó a cabo el modelado y simulación del sistema robótico mediante Diseño Asistido por Computadora (CAD), utilizando el software de ingeniería Autodesk Inventor Professional 2023. **Resultados:** Se obtuvieron las posiciones iniciales y finales del sistema robótico, así como la simulación de movimiento pasivo-continuo. **Conclusiones:** La toma de medidas precisas de un paciente maximiza la posibilidad de implementar un prototipo funcional que contribuya en el proceso de rehabilitación.

**Palabras claves:** Robótica; Rehabilitación; Miembros Inferiores; Diseño; Accidente Cerebro Vascular; Simulación. (Fuente: DeCS-BIREME)

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## INTRODUCTION

In Peru, according to the 2017 Specialized Disability Survey conducted by the Instituto Nacional de Estadística e Informática (INEI), 10.3% of the population, approximately 3,209,261 people, have some form of disability<sup>(1)</sup>. Among these, a total of 10,570 cases of patients with stroke were recorded<sup>(2)</sup>. It is estimated that 60% of people hospitalized due to stroke suffer from disabling sequelae, and only 20% of those affected complete physical rehabilitation programs<sup>(3)</sup>. According to the 2019 INEI data, 88.6% of the total population with some type of disability did not receive treatment or rehabilitation therapy, while only 11.4% managed to access some form of care in this regard<sup>(4)</sup>. This disparity can be partly attributed to the lack of utilization of rehabilitation technology in Peru, due to economic factors and lack of awareness about the existence of these devices as part of physical rehabilitation therapies.

Stroke can be prevented by leading a healthy lifestyle and, if it occurs, can be effectively treated if the patient is taken to a hospital emergency room as soon as possible after presenting the first signs, at which point the chances of recovery are high<sup>(5)</sup>. For the aforementioned reasons, the design of a continuous passive motion robotic system for the rehabilitation of lower limbs in adult patients affected by stroke is proposed. This system aims to facilitate and maximize the recovery of motor functions of the lower extremities, both at home and in hospital settings, with monitoring and follow-up by the rehabilitation physician.

Currently, various studies have been developed to address the diverse mobility problems of the lower limbs, including, for example, the development of systems for gait assistance<sup>(6)</sup>, treatment of motor disabilities caused by cerebral palsy<sup>(7)</sup>, and the development of control applications for exoskeletal systems<sup>(8)</sup>. However, the first models of exoskeletons emerged in the 1960s in the laboratories of Cornell University<sup>(9)</sup>. Yang's structure represents one of the first documented attempts with exoskeletal characteristics, whose primary objective was to increase power in walking rhythm and jumping<sup>(10)</sup>. Another version of this type of exoskeleton was implemented with direct

current motors. However, the motor, power system (battery), and computational technology of the time greatly limited the portability of the device<sup>(11)</sup>.

In Spain, at the Universidad Politécnica de Catalunya, a design of an active knee-ankle orthosis was presented<sup>(12)</sup>. This project focuses on assisting and recovering patients with spinal cord injury, whose condition often leaves them without mobility in approximately 80% of their body. In Latin America, exoskeletons have been developed for the rehabilitation of arms as well as legs. In the field of arm rehabilitation, for example, advances have been made with exoskeletons offering up to four degrees of freedom, adapted to the anthropometry of Mexican patients through optimal conceptual design<sup>(13)</sup>. These exoskeletons focus on the rotation movement of the humerus, flexion and extension of the elbow<sup>(14)</sup>, pronation, and supination of the hand<sup>(15)</sup>. In the case of leg rehabilitation, systems with two degrees of freedom for ankle and knee therapies have been developed, including the use of force, speed, and position sensors<sup>(16)</sup> as well as designs exclusive for knee flexion-extension<sup>(17)</sup>. In this sense, the application of technology in physical rehabilitation improves patient independence when attending their therapies, as demonstrated by research<sup>(18)</sup>.

In conclusion, the development of the project represents a significant advancement in the implementation of rehabilitation equipment that improves the physical condition of patients with gait limitations due to stroke, allowing them to be more independent in their daily activities. In the future, the research aims to implement the lower limb robotic system, providing patients the opportunity to recover an essential component of their function and autonomy under the supervision of the rehabilitation physician.

## METHODS

### Biomechanical analysis of lower limbs

This project focuses on the biomechanical analysis of the lower extremities, which includes the knee and foot as shown in Figure 1, with the purpose of designing a robotic system for the rehabilitation of stroke patients.



The movements and functions of the joints are examined in different contexts to identify specific rehabilitation needs. The critical biomechanical factors to consider in the design of an exoskeleton are the degrees of freedom and movements <sup>(19)</sup>, which

are fundamental for the development of computer-aided design (CAD) modeling that facilitates the recovery of motor function in patients who have experienced a stroke.

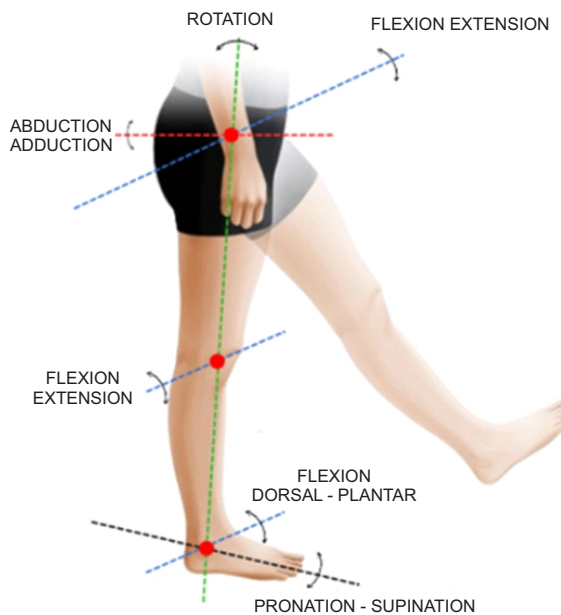


Source: Adapted from [https://www.goconqr.com/es/p/26439765?dont\\_count=true&frame=true&fs=true](https://www.goconqr.com/es/p/26439765?dont_count=true&frame=true&fs=true)

**Figure 1.** Anatomy of the lower limb.

The joints of the lower limb are illustrated, including the hip, knee, and ankle<sup>(20)</sup>, represented by red circles. Lines connect these joints, showing the movement trajectories during the rehabilitation process <sup>(21)</sup>. It can be observed how the system's design allows for

multidirectional movements and personalized adjustments, offering a wide range of exercises to improve mobility and muscle strength in patients with lower limb dysfunction, as shown in Figure 2.



Source: Adapted from <https://www.kenhub.com/es/library/anatomia-es/tipos-de-movimientos-del-cuerpo-humano>

**Figure 2.** Movement of lower limb joints.

According to Table 1, the degrees of biomechanical movement in the knee and ankle joints <sup>(22)</sup> allow the design of robotic rehabilitation systems that can provide personalized and specific therapies for each patient.

The ability to adjust the resistance and speed of movement based on the individual needs of each patient <sup>(23)</sup> is essential for optimizing rehabilitation outcomes and promoting effective recovery of motor function in the lower limbs.

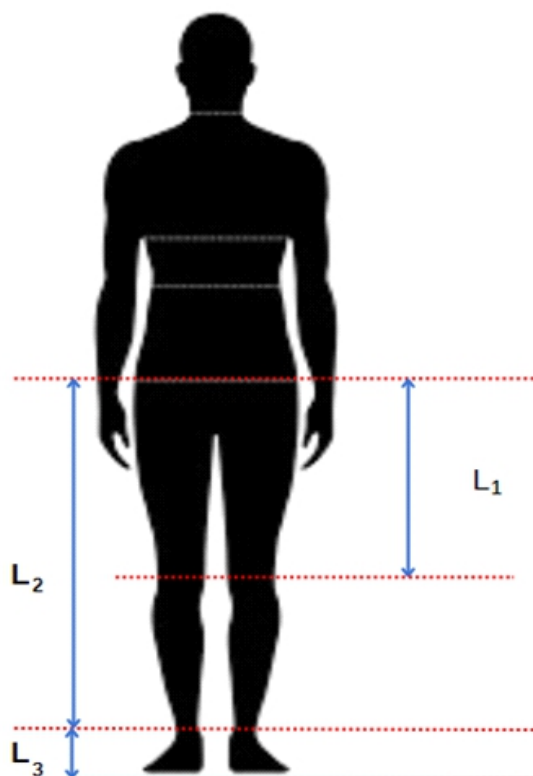
**Table 1.** Degrees of movement of the knee and ankle joint.

Joint	Movement	Degrees
Knee	Extension – Flexion	0° to 120°
Ankle	Plantar – Dorsal Flexion	-40° to 20°
	Supination – Pronation	-35° to 15°

Source: Taken from “Basic Biomechanics of the Musculoskeletal System” (Nordin, 2004).

The measurement of the lower limb was performed by dividing it into L1, L2, and L3 as shown in Figure 3, based on the anatomy and individual proportions of the patient <sup>(24)</sup>. The correct implementation of these anthropometric measurements ensures proper biomechanical alignment and balanced load

distribution during the rehabilitation process, which is essential for maximizing the effectiveness and safety of the treatment. This allows for optimal adjustment to create the CAD prototype design of the lower limb robotic rehabilitation system.



Source: Adapted from <https://depositphotos.com/es/vectors/icono-cuerpo-humano.html>

**Figure 3.** Anthropometric measurements of the lower limb.





Table 2 shows the geometric parameters of the lower limb according to the Denavit-Hartenberg (D-H) convention based on the reference systems and dimensions in Figure 5<sup>(28)</sup>.

**Table 2.** D-H joint parameters for the leg.

Link $i$	$a_i$	$\alpha_i$	$d_i$	$\theta_i$
1	$M_1$	0	0	$\theta_1$
2	$M_2$	0	0	$\theta_2$

Where:

$i$  = represents the joint number

$a_i$  = distance along the  $x_i$

$\alpha_i$  = distance between the  $z_i$  and  $z_{i+1}$

$d_i$  = distance between the  $z_i$

$\theta_i$  = angle between the  $x_i$  and  $x_{i+1}$

The direct kinematic model allows calculating the position and orientation of the leg based on its joint angles.

Therefore, it is necessary to calculate the homogeneous transformation matrix  $A_i$  for each joint, as represented in equation 1.

$$A_i = \begin{bmatrix} \cos(\theta_i) & -\sin(\theta_i) * \cos(\alpha_i) & \sin(\theta_i) * \sin(\alpha_i) & M_i * \cos(\theta_i) & \sin(\theta_i) * \cos(\theta_i) * \cos(\alpha_i) & -\cos(\theta_i) * \sin(\alpha_i) & M_i * \sin(\theta_i) & 0 & \sin(\alpha_i) * \cos(\alpha_i) & d_i & 0 & 0 & 0 & 1 \end{bmatrix} \quad (1)$$

By substituting the joint parameters from Table 2 into equation 1, the following matrices are obtained:

$$A_1 = \begin{bmatrix} \cos(\theta_1) & -\sin(\theta_1) * \cos(\alpha_1) & \sin(\theta_1) * \sin(\alpha_1) & M_1 * \cos(\theta_1) & \sin(\theta_1) * \cos(\theta_1) * \cos(\alpha_1) & -\cos(\theta_1) * \sin(\alpha_1) & M_1 * \sin(\theta_1) & 0 & \sin(\alpha_1) * \cos(\alpha_1) & d_1 & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_1 = \begin{bmatrix} \cos(\theta_1) & -\sin(\theta_1) & 0 & M_1 * \cos(\theta_1) & \sin(\theta_1) * \cos(\theta_1) & 0 & M_1 * \sin(\theta_1) & 0 & 0 & 1 & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_2 = \begin{bmatrix} \cos(\theta_2) & -\sin(\theta_2) * \cos(\alpha_2) & \sin(\theta_2) * \sin(\alpha_2) & M_2 * \cos(\theta_2) & \sin(\theta_2) * \cos(\theta_2) * \cos(\alpha_2) & -\cos(\theta_2) * \sin(\alpha_2) & M_2 * \sin(\theta_2) & 0 & \sin(\alpha_2) * \cos(\alpha_2) & d_2 & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$A_2 = \begin{bmatrix} \cos(\theta_2) & -\sin(\theta_2) & 0 & M_2 * \cos(\theta_2) & \sin(\theta_2) * \cos(\theta_2) & 0 & M_2 * \sin(\theta_2) & 0 & 0 & 1 & 0 & 0 & 0 & 1 \end{bmatrix}$$

To obtain the direct kinematic model (position and orientation of the end) of the lower limb, it is necessary to multiply the matrices  $A_1$  and  $A_2$ .

Therefore, the homogeneous transformation matrix representing the position and orientation is represented in equation 2.

$$T = \begin{bmatrix} \cos(\theta_1 + \theta_2) & -\sin(\theta_1 + \theta_2) & 0 & M_1 * \cos(\theta_1) + M_2 * \cos(\theta_2) & \sin(\theta_1 + \theta_2) * \cos(\theta_1 + \theta_2) & 0 & M_1 * \sin(\theta_1) + M_2 * \cos(\theta_2) & 0 & 0 & 1 & 0 & 0 & 0 & 1 \end{bmatrix} \quad (2)$$

## RESULTS

In the present research, the anthropometric data of a 40-year-old patient were analyzed, as shown in Table 3,

with lower limb limitations due to a stroke, a height of 170 cm, and a weight of 90 kg.

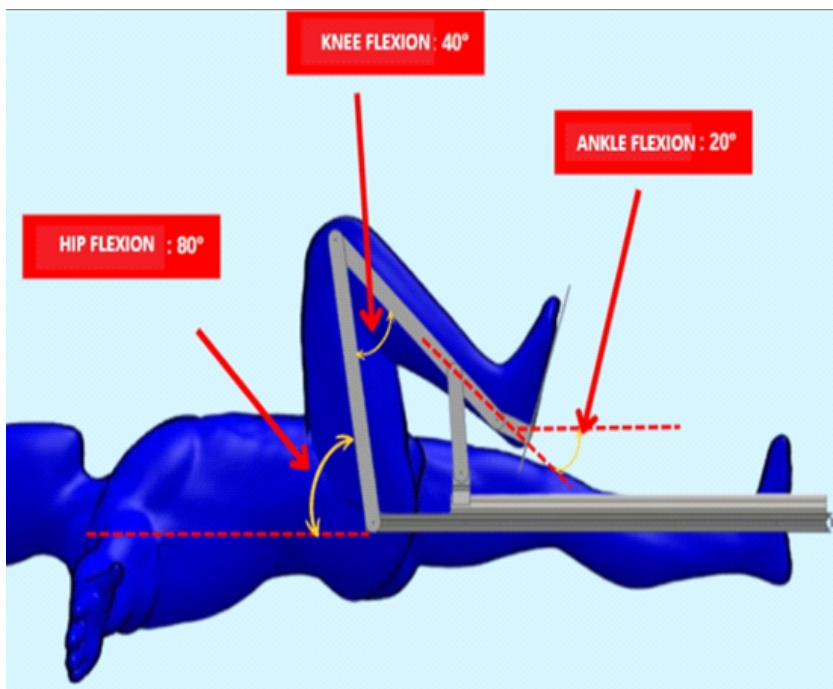
**Table 3.** Lower limb measurements of the patient.

Limb	Dimension (cm)
Thigh	43.01
Leg	41.99
Foot	6.63

ORIGINAL PAPER

The simulation results conducted in Autodesk Inventor Professional 2023 software, as shown in Figure 6, indicate that the robotic system meets the functional requirements for the rehabilitation and improvement of lower limb spasticity in stroke patients. The maximum flexion

movements achieved (80° in the hip, 40° in the knee, and 20° in the ankle) are within the established therapeutic ranges, suggesting that the device can be effective in improving the degrees of movement in these patients, as assessed by the Modified Ashworth Scale<sup>(29)</sup>.

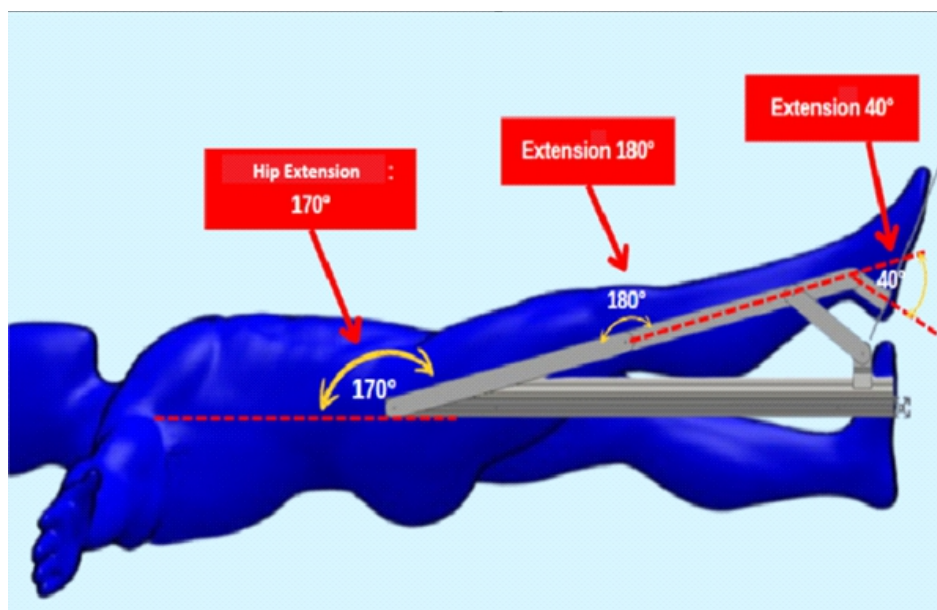


Source: Created in Autodesk Inventor Professional 2023.

**Figure 6.** Simulation of the robotic system in flexion.

For knee extension, the system successfully reached 180°, representing full extension. This range is crucial for facilitating natural movements and daily activities such as walking, standing up, and sitting down. The simulation showed that the knee mechanism can support the load without compromising stability, which is essential for effective rehabilitation.

The precision in the simulation suggests that the system can replicate physiological movements with high fidelity, which is essential to avoid injuries and maximize therapy effectiveness. Additionally, the system's stability under maximum extension conditions ensures that patients can use it safely during prolonged rehabilitation sessions.



Source: Created in Autodesk Inventor Professional 2023.

**Figure 7.** Simulation of the robotic system in extension.

The maximum extension angles achieved in the hip ( $170^\circ$ ), knee ( $180^\circ$ ), and ankle ( $40^\circ$ ), as shown in Table 4, are adequate to facilitate comprehensive functional recovery.

These results support the use of this system as a potentially valuable tool in physical rehabilitation programs, contributing to improved quality of life for patients.

**Table 4.** Lower limb measurements of the patient.

Limb	Figure 7	Figure 8
Cadera	$80^\circ$	$170^\circ$
Rodilla	$40^\circ$	$180^\circ$
Tobillo	$20^\circ$	$40^\circ$

The precision in the simulation suggests that the system can replicate physiological movements with high fidelity, which is essential to avoid injuries and maximize therapy effectiveness.

## CONCLUSIONS

This research demonstrates that the lower limb medical robotic system<sup>(30)</sup> has been designed with biomechanical principles and simulated using the Denavit-Hartenberg (D-H) algorithm, showing its potential to be a valuable tool in the rehabilitation of stroke patients by providing knee and ankle movements essential for functional recovery. Additionally, the homogeneous transformation matrices

enable the creation of displacement graphs and simulations of leg movement, providing better understanding and control of the rehabilitation process.

The extension and flexion angles achieved by the system are adequate to facilitate comprehensive recovery. The system's ability to maintain these angles stably and controlled ensures that patients can perform the necessary rehabilitation exercises without risk of injury, which is essential for safe and effective therapy, thereby significantly improving the quality of life for stroke patients. The results obtained not only confirm the conceptualization of the system's technical feasibility but





also open the possibility of developing real prototypes and evaluating them in clinical settings. Moreover, this project has the potential to be used in future space missions where lower limb rehabilitation is required, as muscle deterioration occurs in low-gravity environments<sup>(31)</sup>. As future work, it is proposed to implement and test the

prototype, conducting spasticity evaluations on the Modified Ashworth Scale before and after using the device in a group of stroke patients to validate its in-situ effectiveness and optimize the design to an ergonomic model. The next stage of the project, which will involve use in humans, will have the approval of the Ethics Committee.

**Authorship contribution:** C.M.C. and C.S. participated in the conceptualization, research, methodology, data analysis and interpretation, resources, and writing of the original draft; J.B.A. participated in clinical supervision and application of results; R.P., M.M.M., and J.C. participated in technical supervision and advice, data analysis and interpretation, writing of the article, and critical revision of the article.

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